Fermilab

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Wideband Control for Magnetron Driven Cavities

Brian Chase - Fermilab
Michael Read - Calabazas Creek Research Inc

Magnetron Collaboration

- Calabazas Creek Research Inc
  - Michael Read, R. Lawrence Ives, Thuc Bui
- Fermi National Accelerator Laboratory
  - Brian Chase, Ralph Pasquinelli, Ed Cullerton, Philip Varghese Josh Einstein, John Reid
- Communications and Power Industries LLC
  - Chris Walker, Jeff Conant
- Previous Collaboration with Muon's Inc.

  Gregory Kazakevitch

Outline

- Demands for high power, high efficiency RF
- Vector control schemes for magnetrons
- Experimental results
- Ongoing research

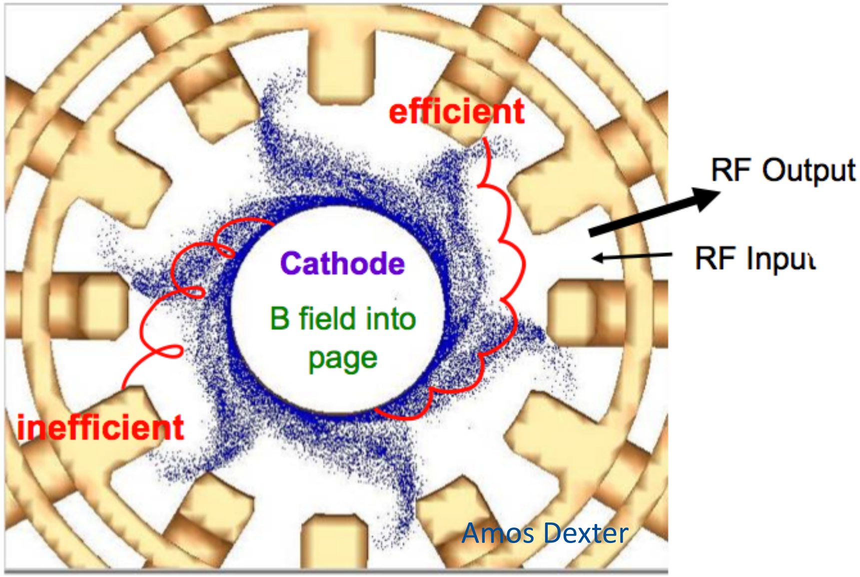
Take-a-ways from the Proton Driver High Efficiency Workshop at PSI

- **Proton Drivers**:
  - GeV-energy range
  - MW-beam power range
- Applications: neutrinos, muons, neutrons, Accelerator Driven Systems(ADS).
- **Types of accelerators for proton drivers:**
  - Cyclotrons and Fixed-Field Alternating Gradient accelerators (FFAG);
  - Rapid Cycle Synchrotrons (RCS);
  - High intensity pulsed linear accelerators;
  - CW Superconducting RF linear accelerators.
- **High RF efficiency is critical for high beam power application**

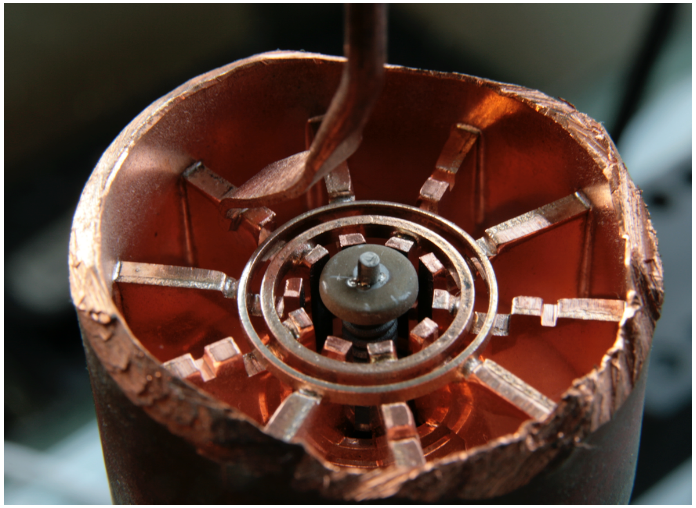
The basics of magnetron operation

Cathode at negative potential accelerates electrons outward.
B field causes electrons to spiral
E field across gaps causes bunching into electron cloud spokes. Rotating spokes intern excites cavities. RF power is coupled out and is constant amplitude.

Injection Locking:
RF maybe driven in on same port and cause the spokes to phase lock up to source providing low noise RF



Amos Dexter



Cross section of a cooker magnetron showing cathode and RF cavities

R. Adler, A study of locking phenomena in oscillators, Proc. IRE and Waves and Electrons, vol. 61, no. 10, pp. 351-357, June 1946.

Magnetrons excel at many RF source requirements

- Power: >100 kW CW and MW scale pulsed operation
  - average power capability increase with lower frequency
- Efficiency: High power devices > 85% at L-band
- Power supply voltage: typically < 25kV
- Low cost: $0.50/watt at 100kW and 50 units
- Small size: 100 kW pulsed 1300 MHz tube is <1 foot high and does not require an oil tank
- They are easy to replace and rebuild and can be designed for a reasonably long life and low noise when injection locked
- However, they are basically a constant power device, not a linear amplifier like a klystron

Industrial CW Magnetrons

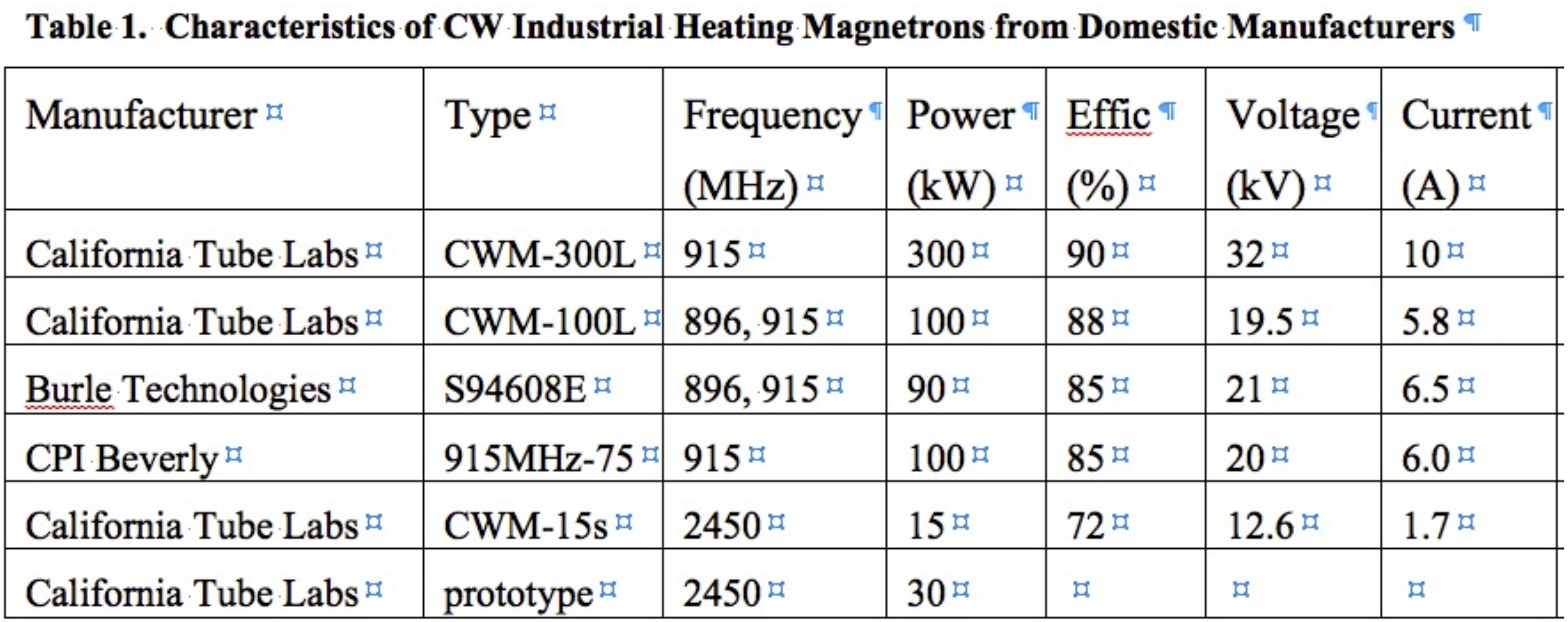


Table 1. Characteristics of CW Industrial Heating Magnetrons from Domestic Manufacturers

Manufacturer	Type	Frequency (MHz)	Power (kW)	Effic (%)	Voltage (kV)	Current (A)
California Tube Labs	CWM-300L	915	300	90	32	10
California Tube Labs	CWM-100L	896, 915	100	88	19.5	5.8
Burle Technologies	S94608E	896, 915	90	85	21	6.5
CPI Beverly	915MHz-75	915	100	85	20	6.0
California Tube Labs	CWM-15s	2450	15	72	12.6	1.7
California Tube Labs	prototype	2450	30			

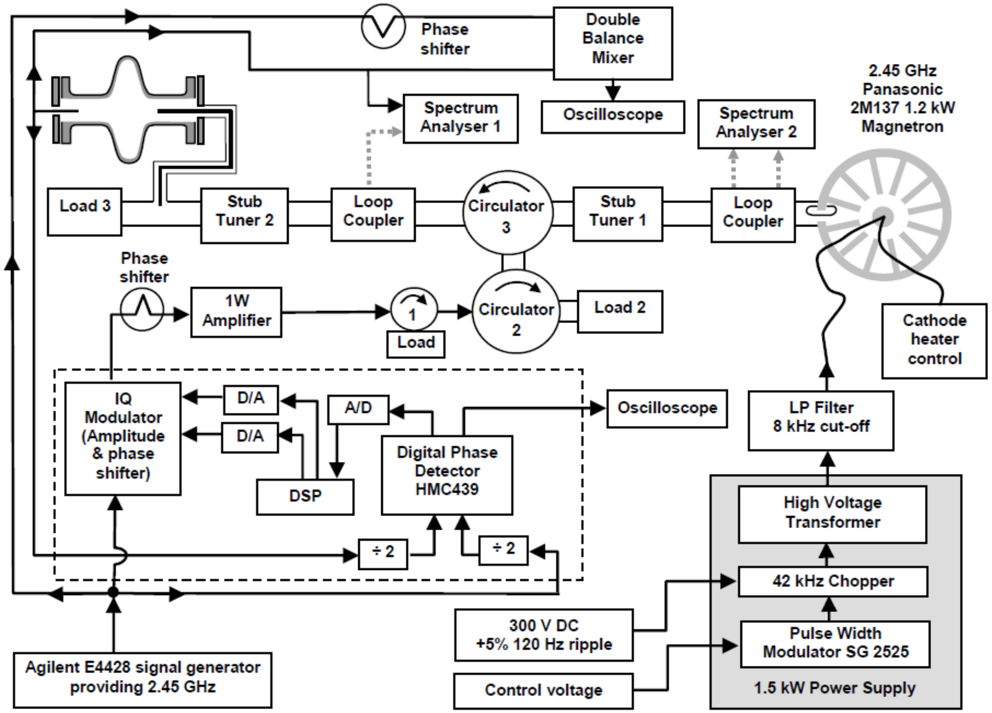
- High power CW magnetrons used for industrial heating are catalog items
- > 85% efficiency typical
- 100 kW L-band - 18” length, 5” diameter

Phase control loop around SRF cavity

Lancaster: Amos Dexter, Graeme Burt and Chris Lingwood

Demonstration of CW 2.45 GHz magnetron driving a specially manufactured superconducting cavity in a VTF at Jlab.

Control of phase in the presence of microphonics was successful.



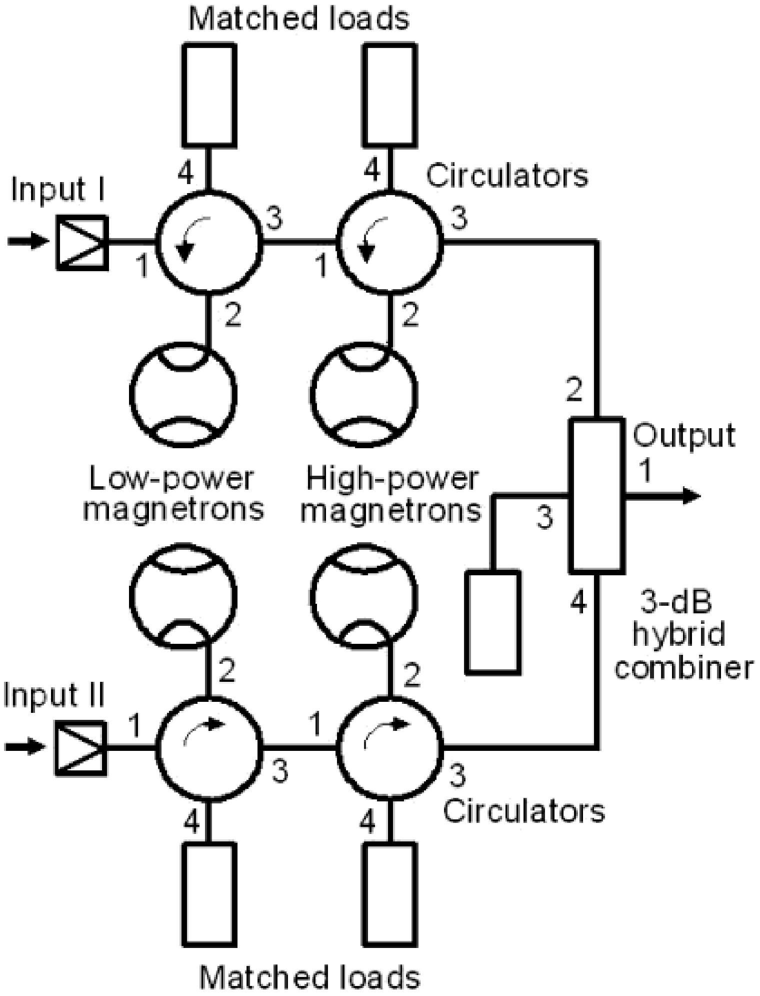
H. Wang *et al.*, “USE OF AN INJECTION LOCKED MAGNETRON TO DRIVE A SUPERCONDUCTING RF CAVITY,” in *Proceedings of IPAC’10*, Kyoto, Japan, THPEB067.

Cascaded magnetrons and out-phasing AM control

Concept: cascade injection locked magnetrons to increase gain, combine two pairs to get amplitude control by outphasing in pulsed mode operation

Outcome: Proof of concept for cascade stage and the realization that we needed CW power supplies to make real progress. Strong belief that this scheme would work but it does have its complexities.

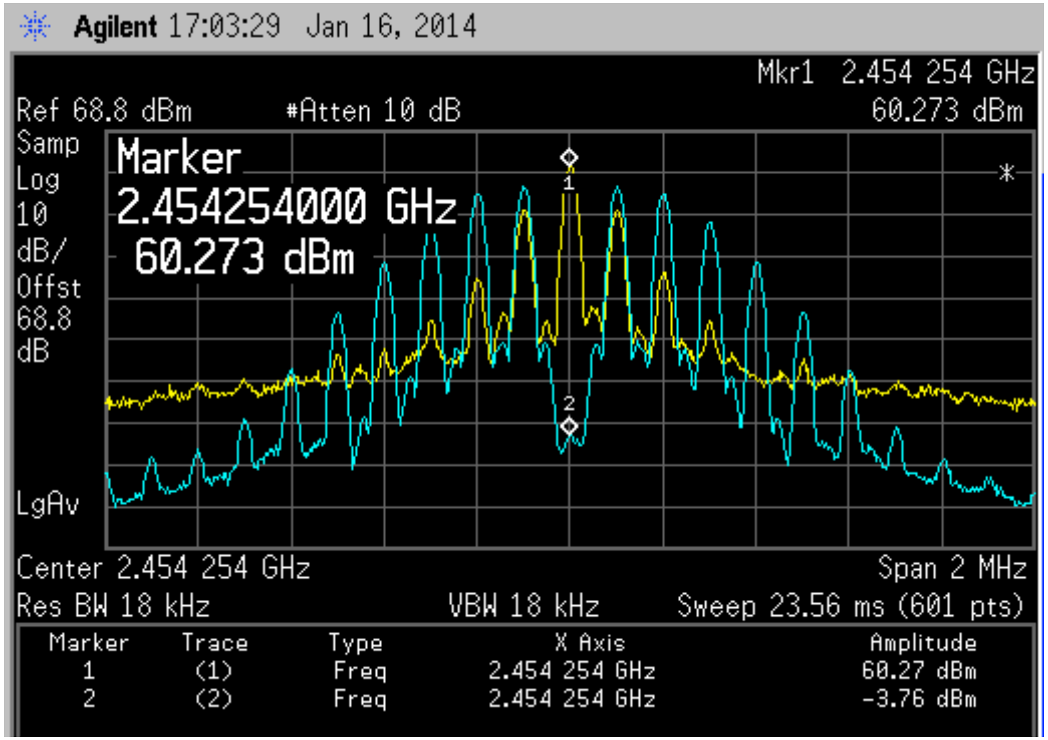
Grigory Kazakevich, et al. Muons Inc.
Yakovlev, Pasquinelli, Chase, et al. Fermilab



Amplitude control by fast phase modulation technique

Magnetrons are constant output power devices. However, the power in the carrier destined for the cavity can be reduced by fast phase modulation, moving power from the carrier into discreet Bessel sidebands that are outside the cavity bandwidth. These sidebands will be reflected from the cavity and back to the circulator load

Increasing the modulation depth(137 degrees) suppresses the carrier over a measured 64 dB dynamic range in lab

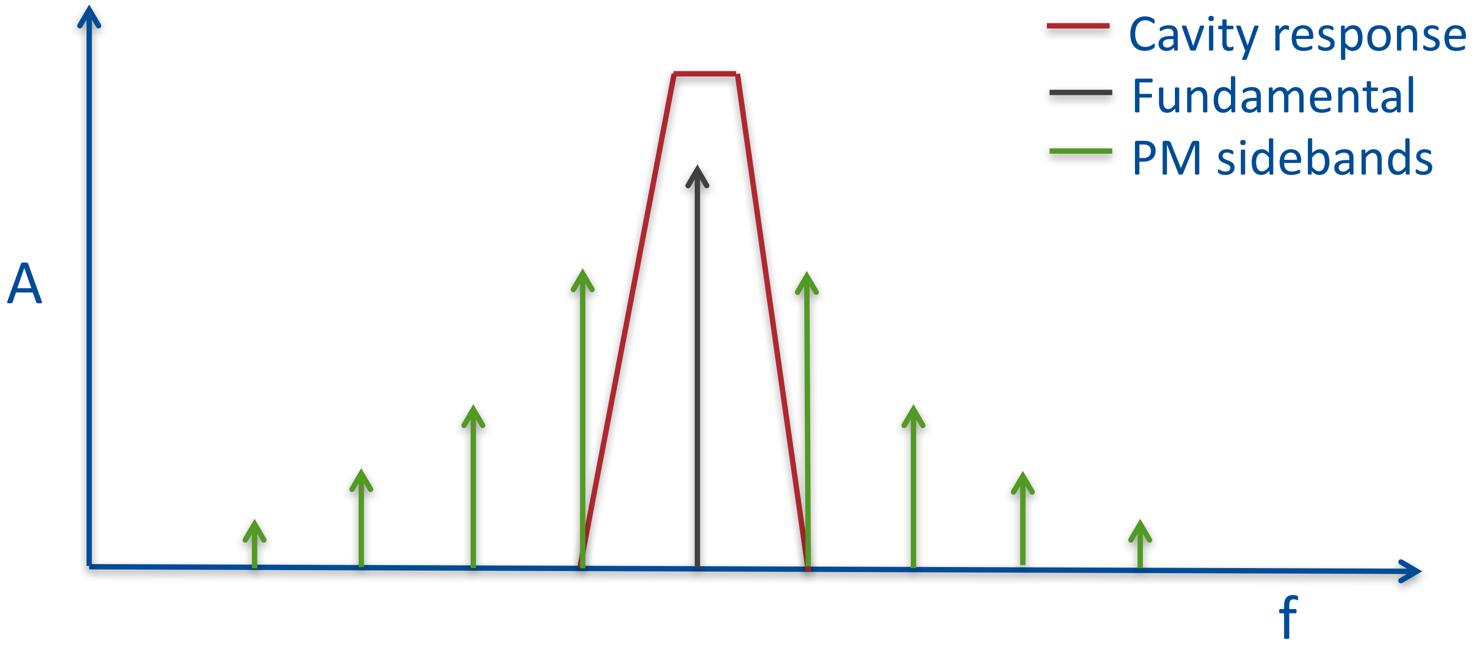


```
Agilent 17:03:29  Jan 16, 2014
                                          Mkr1  2.454 254 GHz
Ref 68.8 dBm        #Atten 10 dB                  60.273 dBm
Samp   Marker
Log    2.454254000 GHz
10      60.273 dBm
dB/
Offst
68.8
dB

LgAv
Center 2.454 254 GHz                                 Span 2 MHz
Res BW 18 kHz             VBW 18 kHz     Sweep 23.56 ms (601 pts)
  Marker     Trace     Type       X Axis              Amplitude
    1         (1)      Freq    2.454 254 GHz          60.27 dBm
    2         (2)      Freq    2.454 254 GHz          -3.76 dBm
```

Rejection of PM sidebands by Narrowband Cavity

While output power is constant, sinusoidal phase modulation creates discrete sidebands at multiples of the modulation frequency while the power shifted from carrier to sidebands is determined by modulation depth



Phase Modulation Equations

$$Acos(\omega_C t + bsin\omega_M t) = AJ_0(\beta)cos\omega_C t +$$

$$\sum_{k=1}^{\infty} J_{2k}(\beta)[sin(\omega_C + 2k\omega_M)t + sin(\omega_C - 2k\omega_M)t] +$$

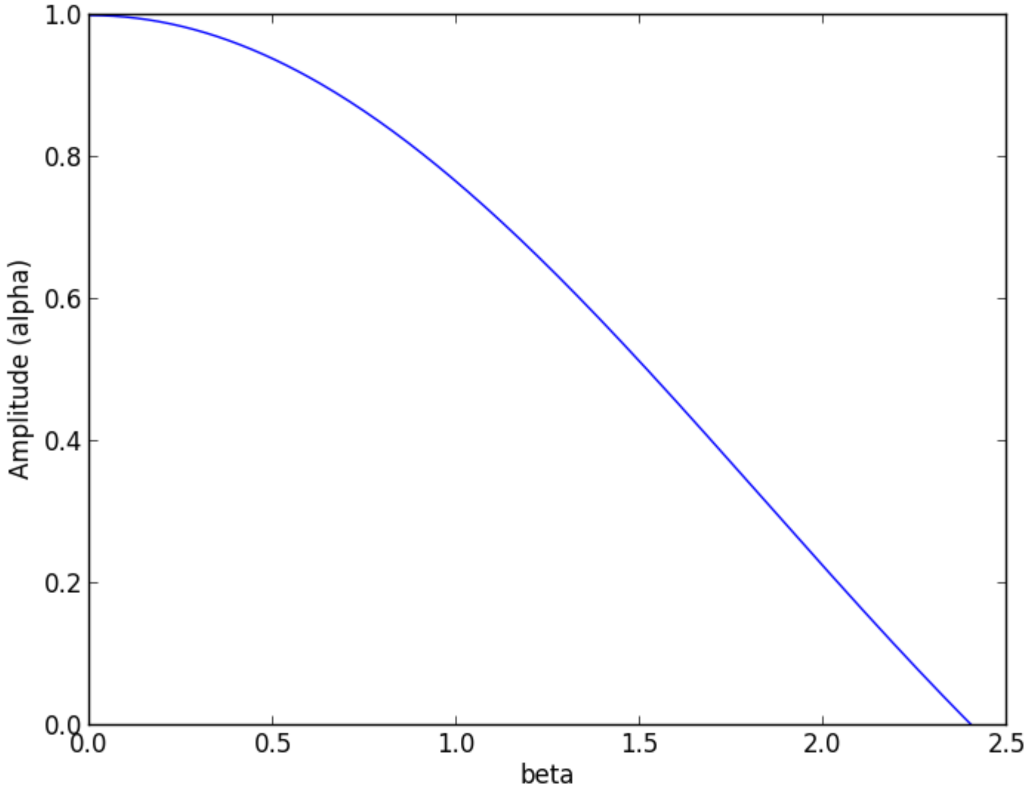
$$\sum_{k=0}^{\infty} J_{2k+1}(\beta)[cos(\omega_C + (2k+1)\omega_M)t - cos(\omega_C - (2k+1)\omega_M)t]$$

$$J_0(\beta) = 1 - \frac{\beta^2}{2^2} + \frac{\beta^4}{2^2.4^2} - \frac{\beta^6}{2^2.4^2.6^2} + ...$$

Used for generation of amplitude-to-phase LUT. Generates a lookup table such that the region Before the first null in the Bessel is covered by the controller. Allows for linearization corrections by just adding a scaling table.

$$J_0(\beta) - \alpha = 0$$

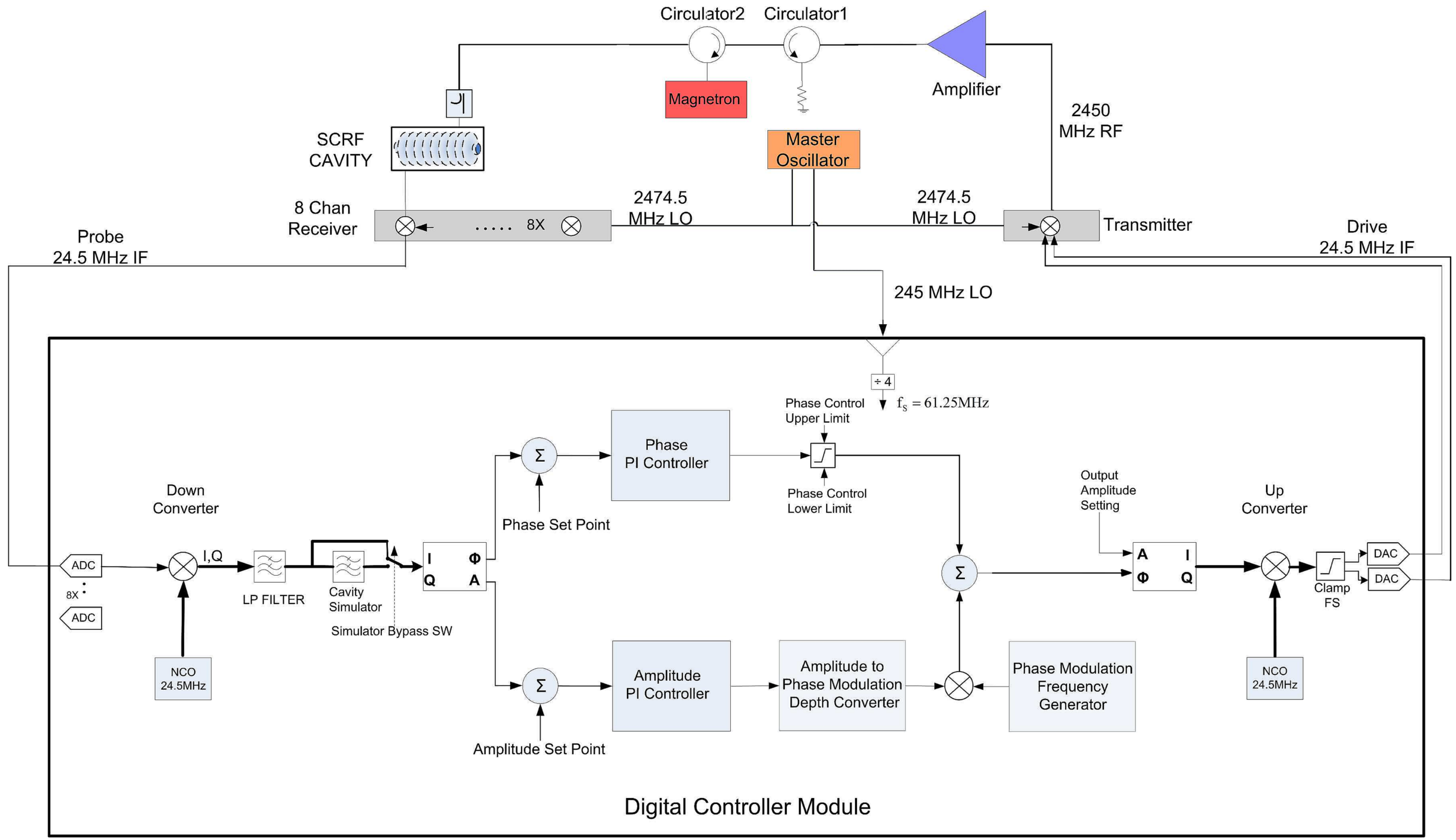
Bessel of the first kind, Region before first null



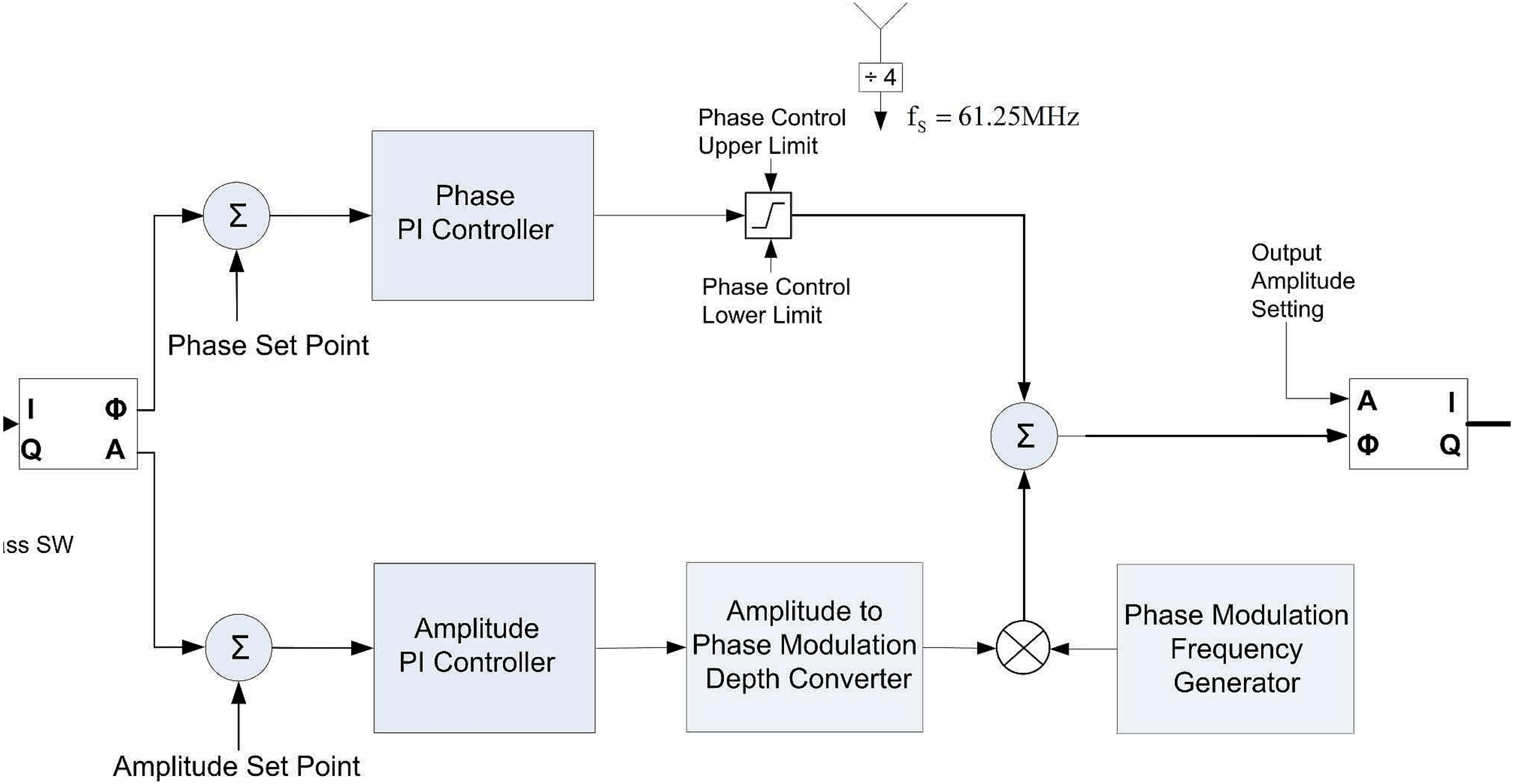
Inverse function in look up table drives phase modulation depth to linearize cavity drive

LLRF controller for 2.45 GHz SRF cavity driven by 1.2 kW Magnetron using Fast Phase Modulation

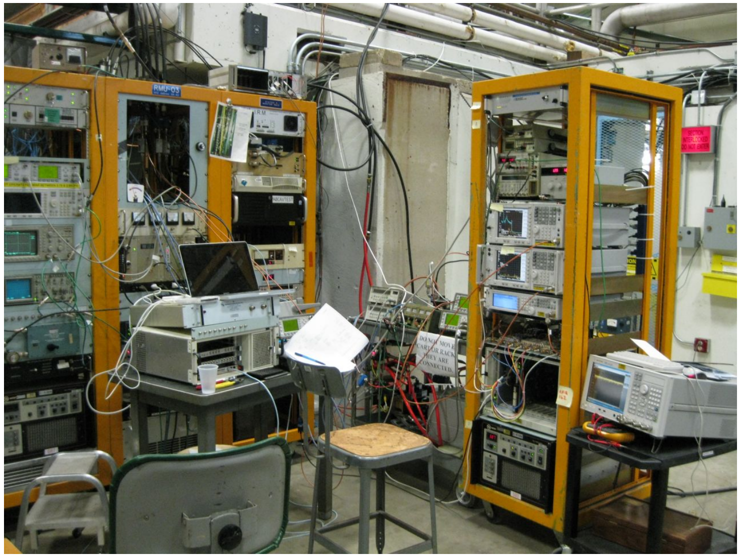
Magnetron Amplitude and Phase Control System



Controller architecture



Injection Locked 2.45 GHz magnetron driving SRF cavity



Commercially procured 2.45 GHz 1.2 kW magnetron

Loaned SRF cavity from JLab

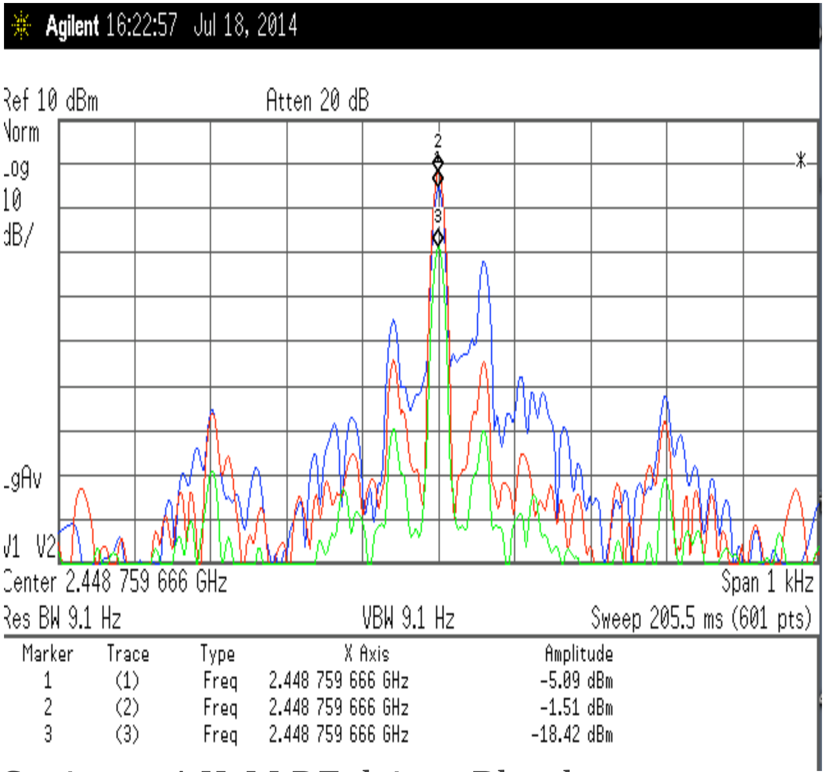
Testing took place over one week period in July 2014.

Published in JINST

A0 VTS 2.4 GHz Magnetron - Cavity test results

- Amplitude control shown linear over 30 dB range
- Moderate feedback performance demonstrated
- 0.3% r.m.s, and phase stability of 0.26 degrees r.m.s.

- Tests limited by extreme cavity microphonics and very limited time with the test cave

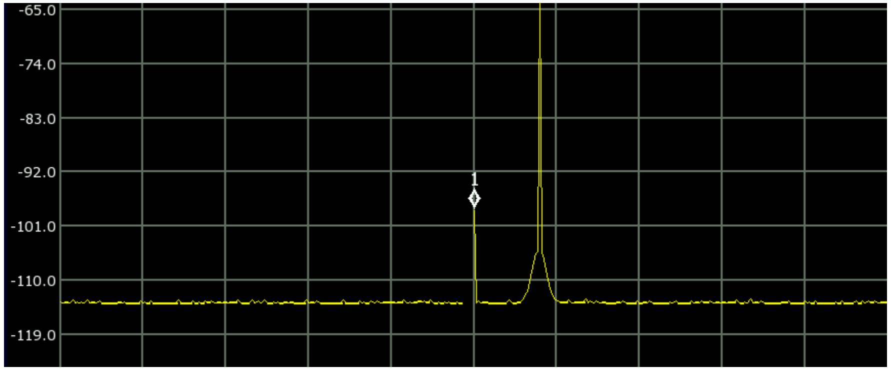


Marker	Trace	Type	X Axis	Amplitude
1	(1)	Freq	2.448 759 666 GHz	-5.09 dBm
2	(2)	Freq	2.448 759 666 GHz	-1.51 dBm
3	(3)	Freq	2.448 759 666 GHz	-18.42 dBm

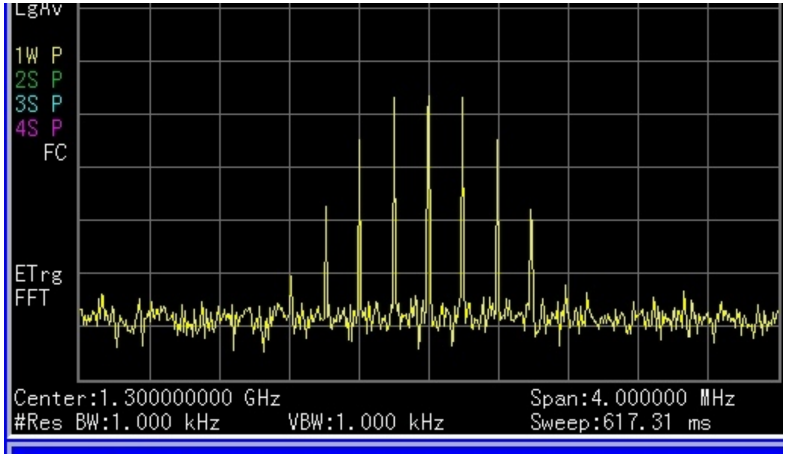
Cavity at 4 K, LLRF drive. Blue loops open, Red loops closed and maximum output, Green loops closed and amplitude reduced by 17 dB shows the PM modulation is effective for amplitude control.

Phase Modulation Tests on 1300 MHz 9-cell Cavity

- 9 cell cavity is driven by a phase modulated source through a 4kW solid state amplifier

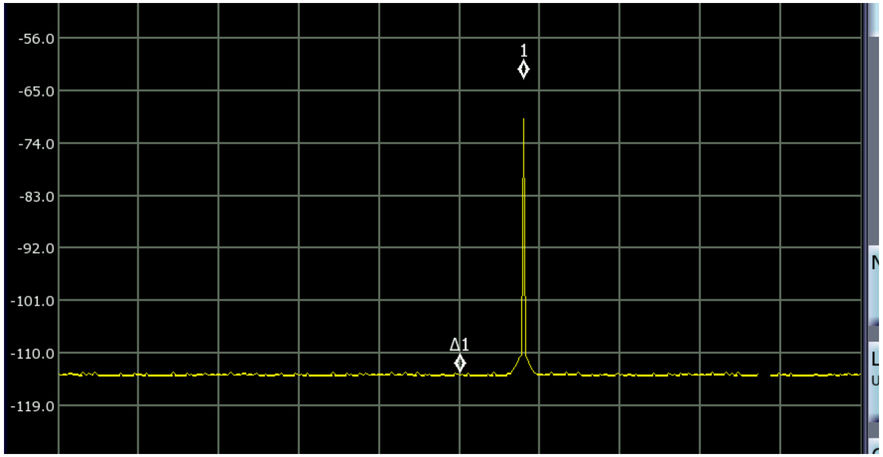


8/9 pi mode driven by carefully tuned 2nd sideband



Center:1.300000000 GHz Span:4.000000 MHz
#Res BW:1.000 kHz VBW:1.000 kHz Sweep:617.31 ms

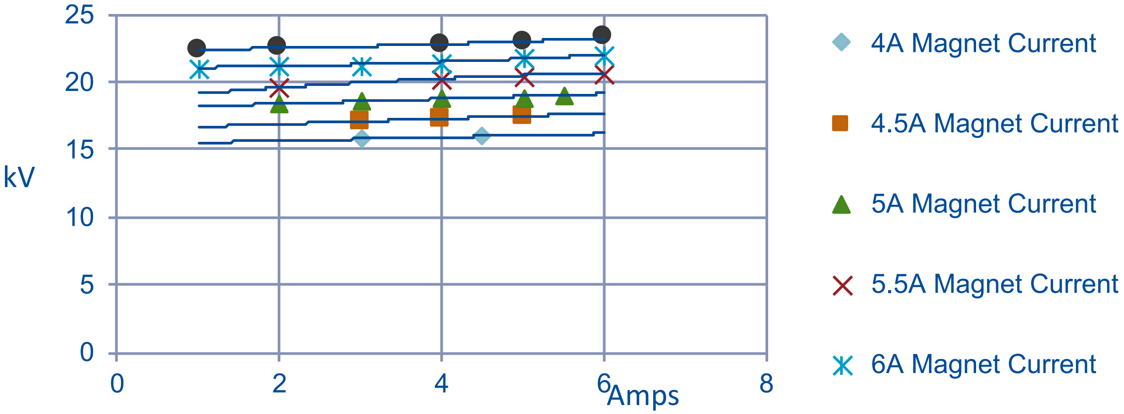
Forward power from SSA



8/9 pi mode is easily not excited by sidebands

CCR / CPI - 100 kW Pulsed, 10 kW Ave. 1.3 GHz Magnetron

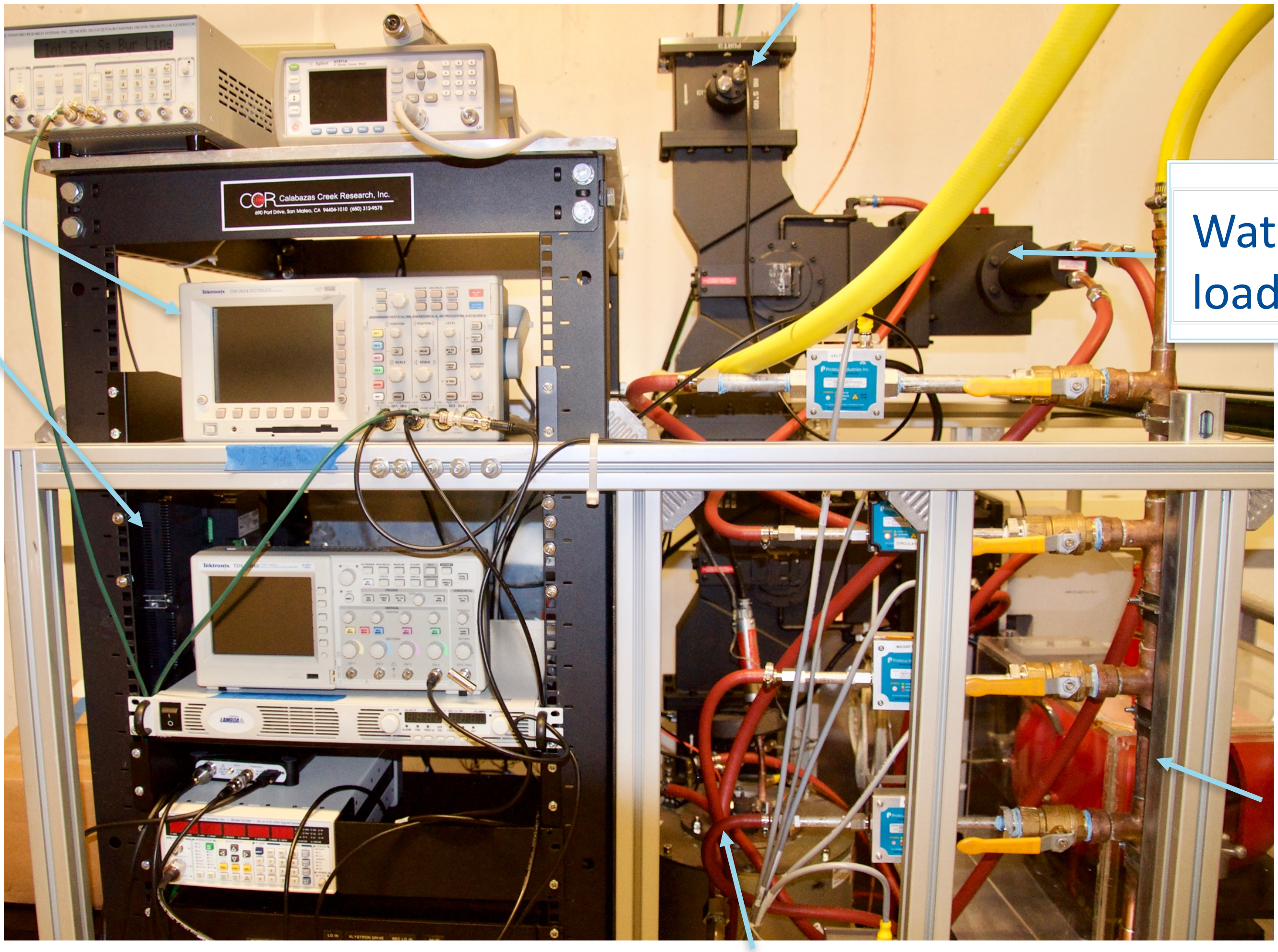
Calabazas Creek Research Inc
Phase II SBIR grant to develop a 1.3 GHz, 100 kW peak power, 10 kW average power magnetron station in partnership with Fermilab and Communications and Power Industries LLC, utilizing a full vector control scheme developed by Fermilab.



V-I Characteristics of Magnetron at Varying Electromagnet Current
Values from initial short pulse tests.

tube~12” tall

CCR 1.3 GHz 100 kW magnetron testing at HTS Fermilab



Isolator with shorting plate

Diagnostics and control

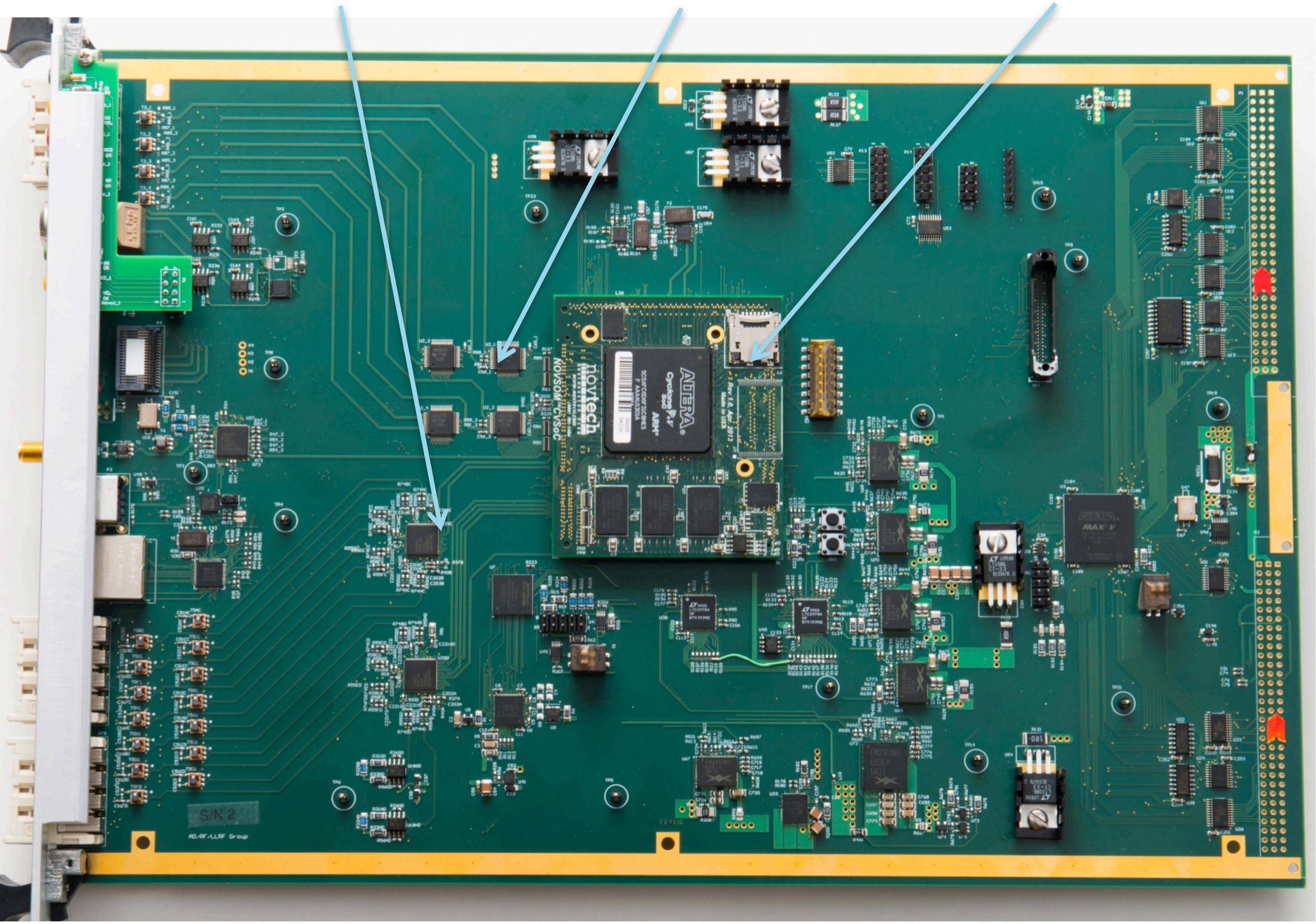
Water cooled load

High voltage modulator not shown

Klystron

100 kW Magnetron

LLRF Digital Control Card for Phase Modulation Scheme



(16) 14 bit ADCs (8)14 bit DACs System on Module

Dual core Arm processor
with FPGA eliminates the need for a crate and external processor.

Testing Status

- Magnetron cart shipping and installed at HTS
  - Water cooling, 208VAC power, high voltage pulsed modulator cabled
- 5 kW klystron CW powered up and driven with pulsed RF
  - Ready for safety review and testing with 22 kV modulator
- Near term plans are to fully characterize the injection locked magnetron
  - Power curves and efficiency
  - Magnetron self heating as a function of modulation depth and frequency
  - Power supply sensitivity
- Drive 9-cell cavity when available

Magnetron Control R&D moving forward

- Cathode current control is a logical choice for slow amplitude control to optimize efficiency for operating conditions
  - there is potential for moderate bandwidth with switch-mode PS
  - should be a part of any scheme
- Vector addition and out-phasing of two magnetrons should work for most designs
  - at the cost of hardware complexity and moderate control complexity
- RF vector control through fast phase modulation is a potential fit for many machine designs
  - single tube design with greatest hardware simplicity
  - at the cost of control complexity
- All techniques need development time on a stable test platform

Summary

- The magnetron has been a remarkable RF source for 75 years that is unparalleled in cost and highly efficient. It is widely used for industrial heating and smaller electron accelerators but has had little impact in hadron accelerators
- There are now several control architectures that can take advantage of the processing capabilities of modern FPGAs
- Testing is in progress with1.3 GHz 100 kW 10% duty factor magnetron and controller using fast phase modulation.
- Magnetrons may be a strong contender for high power, high efficiency accelerators

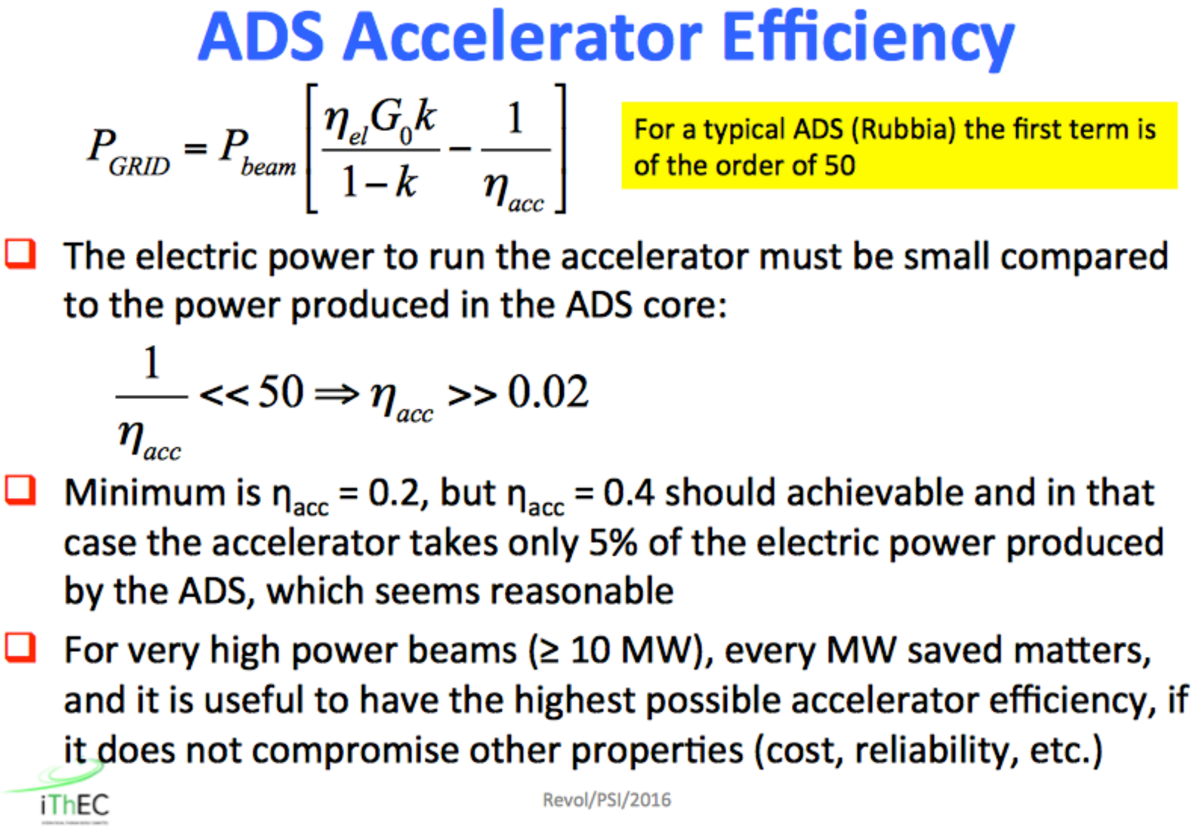
Thank you for your attention!

Backup slides

References

- B. Chase, R. Pasquinelli, E. Cullerton, and P. Varghese, “Precision Vector Control of a Superconducting RF Cavity driven by an Injection Locked Magnetron,” *Journal of Instrumentation*, no. 10 P03007, 2015.
- H. Wang *et al.*, “USE OF AN INJECTION LOCKED MAGNETRON TO DRIVE A SUPERCONDUCTING RF CAVITY,” in *Proceedings of IPAC’10*, Kyoto, Japan, THPEB067.

Efficiency Goals



ADS Accelerator Efficiency

$$P_{GRID} = P_{beam}\left[\frac{\eta_{el} G_0 k}{1-k} - \frac{1}{\eta_{acc}}\right]$$

For a typical ADS (Rubbia) the first term is of the order of 50

- ☐ The electric power to run the accelerator must be small compared to the power produced in the ADS core:

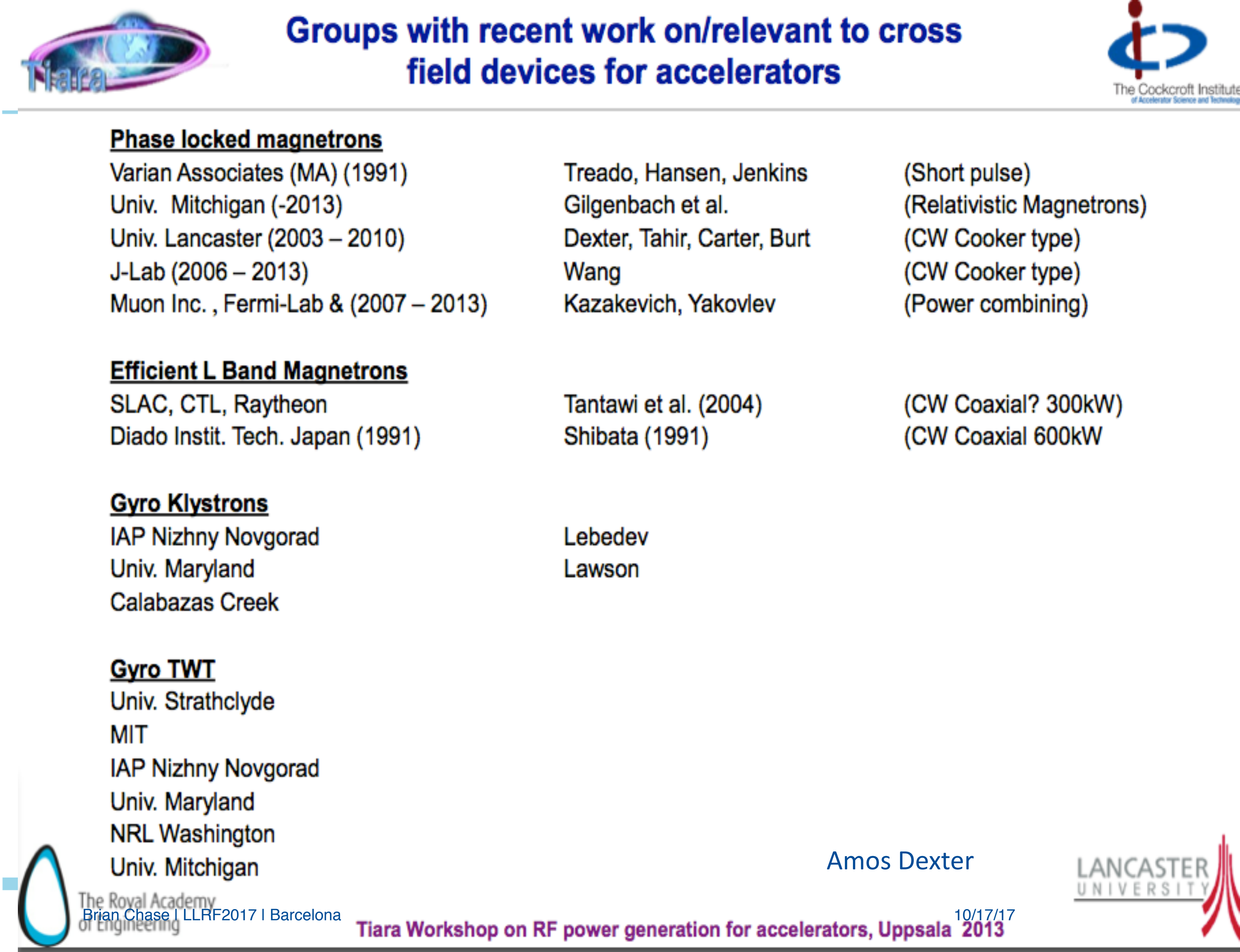
$$\frac{1}{\eta_{acc}} << 50 \Rightarrow \eta_{acc} >> 0.02$$

- ☐ Minimum is $\eta_{acc} = 0.2$, but $\eta_{acc} = 0.4$ should achievable and in that case the accelerator takes only 5% of the electric power produced by the ADS, which seems reasonable
- ☐ For very high power beams (≥ 10 MW), every MW saved matters, and it is useful to have the highest possible accelerator efficiency, if it does not compromise other properties (cost, reliability, etc.)

iThEC

Revol/PSI/2016

- For high power SRF linacs the RF sources are a key component in overall wall-plug efficiency



Groups with recent work on/relevant to cross field devices for accelerators

Phase locked magnetrons

Varian Associates (MA) (1991)	Treado, Hansen, Jenkins	(Short pulse)
Univ. Mitchigan (-2013)	Gilgenbach et al.	(Relativistic Magnetrons)
Univ. Lancaster (2003 – 2010)	Dexter, Tahir, Carter, Burt	(CW Cooker type)
J-Lab (2006 – 2013)	Wang	(CW Cooker type)
Muon Inc. , Fermi-Lab & (2007 – 2013)	Kazakevich, Yakovlev	(Power combining)

Efficient L Band Magnetrons

SLAC, CTL, Raytheon	Tantawi et al. (2004)	(CW Coaxial? 300kW)
Diado Instit. Tech. Japan (1991)	Shibata (1991)	(CW Coaxial 600kW

Gyro Klystrons

IAP Nizhny Novgorad	Lebedev
Univ. Maryland	Lawson
Calabazas Creek	

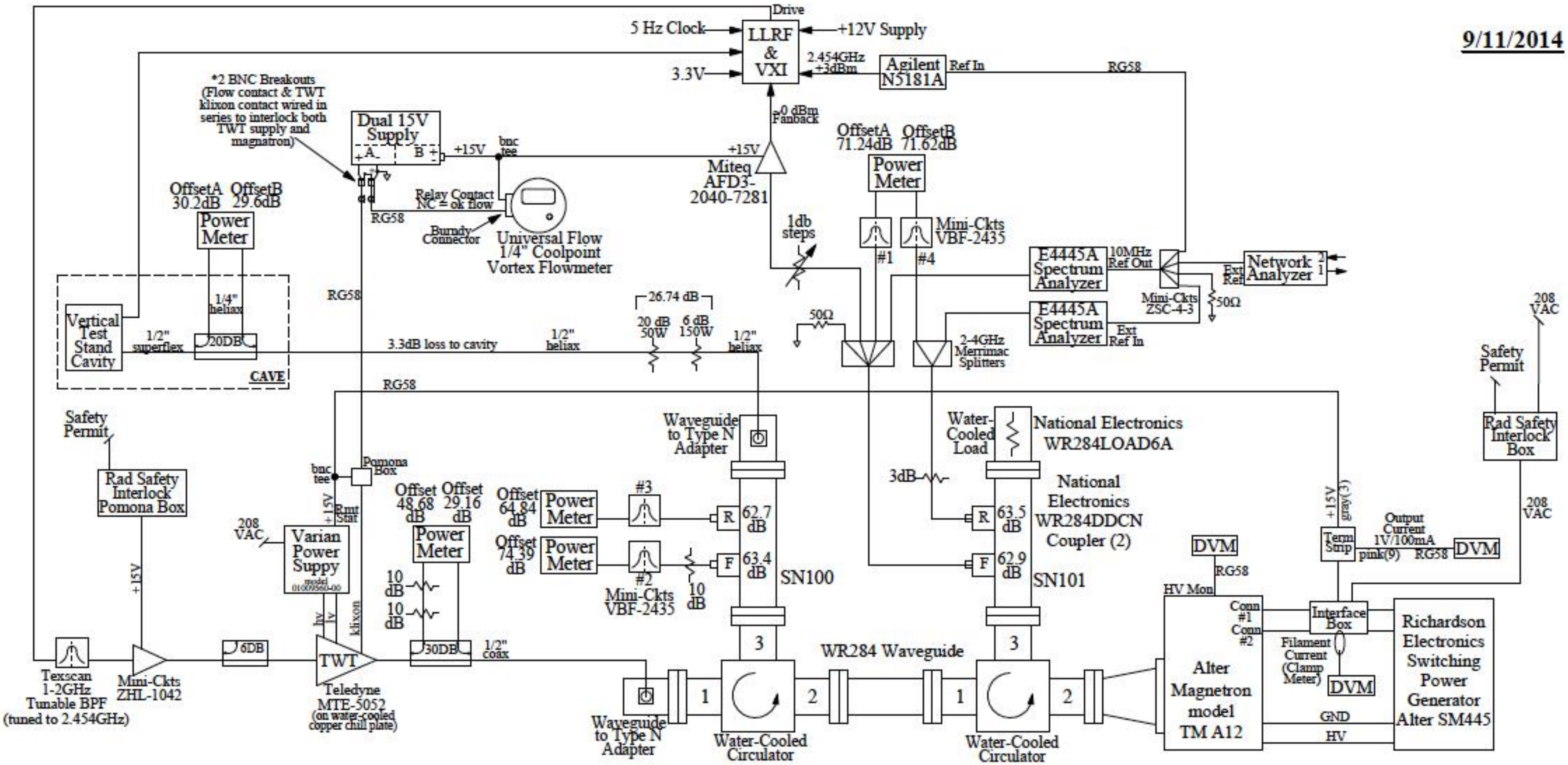
Gyro TWT

- Univ. Strathclyde
- MIT
- IAP Nizhny Novgorad
- Univ. Maryland
- NRL Washington
- Univ. Mitchigan

Amos Dexter

Tiara Workshop on RF power generation for accelerators, Uppsala 2013

A0 Vertical test stand, Jlab 2.45 GHz single cell undressed cavity RF block diagram



1950s transmitter using 2 magnetrons and out-phasing

Patent awarded in 1952 for a transmitter design using cathode voltage modulation and out-phasing with two magnetrons

Why was this technology discarded?
- Possibly just too many parts and expense.

Dec. 2, 1952 J. S. DONAL, JR 2,620,467

AMPLITUDE MODULATION OF MAGNETRONS

Filed Jan. 25, 1950 5 Sheets-Sheet 3

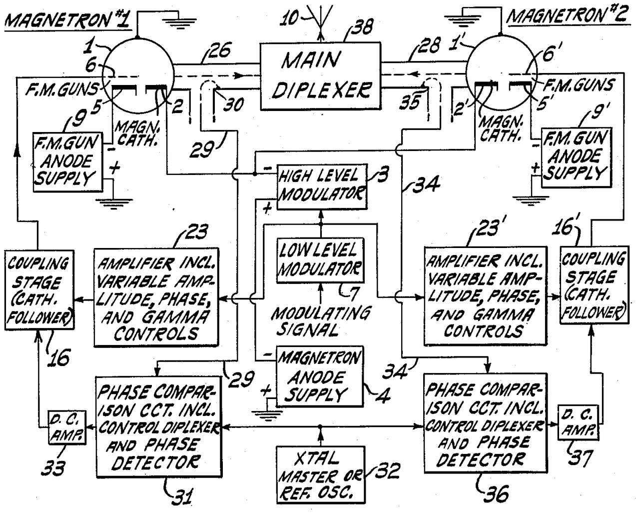


Fig_6

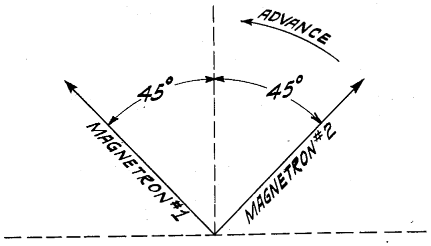


Fig_7

INVENTOR
John S. Donal, Jr.
BY Harry Tunick
ATTORNEY