

A study of undulator magnet characterization using the vibrating wire technique

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A. Temnykh et al., Nucl. Instr. And Meth. A622 (2010) 650-656

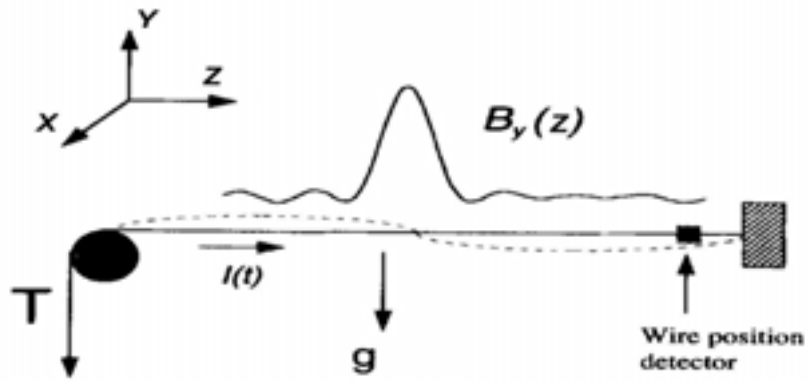
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Outline

- Introduction
- Measurement principle
- Test set-up
- Experiments and results
 - Repeatability test
 - Measurement of localized field distortion
 - Sensitivity to local field errors
 - Vibrating wire vs. Hall probe
- Conclusion

Introduction



$$\mu \frac{\partial^2 Y}{\partial t^2} = T \frac{\partial^2 Y}{\partial z^2} - \gamma \frac{\partial Y}{\partial t} - \mu g + B_y \cdot I_0 \exp(i\omega t)$$

- Magnetic field sensing element - stretched wire
- Amplitudes and phases of various vibrating modes depend on field distribution
- Driving current as a reference for lock-in wire motion detection
- Magnetic field could be reconstructed from the measurements (details in *)

Applications

- Successfully used for finding magnetic axis and alignment
- Small gap/bore undulators
- Quick check of field integrals in the tunnel with limited access to the tested field
- Elliptical and variable polarization undulators



* A. Temnykh, Nucl. Instr. And Meth., 399 (1997) 185.
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Measurement principle

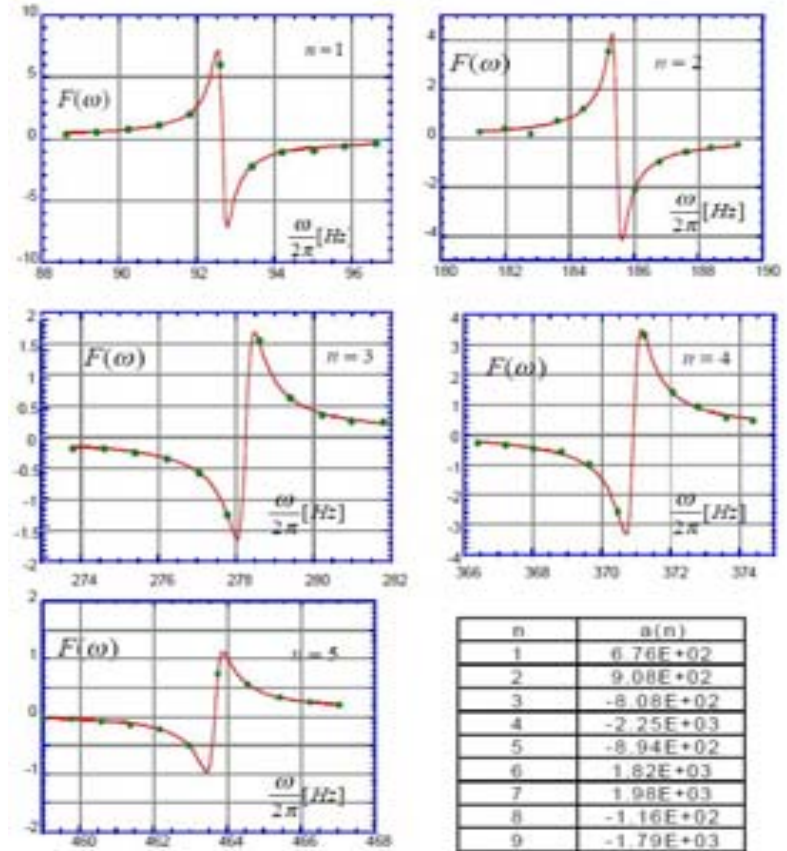
$$Y_{\vec{a}}(z, t) = \frac{1}{\mu} \sum_{n=1}^{\infty} \frac{B_n \sin\left(\frac{\pi n}{L} z\right)}{(\omega^2 - \omega_n^2 + i\gamma\omega)} I_0 \exp(i\omega t)$$

$$F(\omega) = \sum_{n=1}^{\infty} \frac{B_n I_0^2}{2\mu} \sin\left(\frac{\pi n}{L} z_s\right) \frac{(\omega - \omega_n)}{4\omega(\omega - \omega_n)^2 + \omega\gamma^2}$$

$$F(\omega) = F_n(\omega) = a_n \frac{(\omega - \omega_n)}{4\omega(\omega - \omega_n)^2 + \omega\gamma^2}$$

$$B_n = a_n \frac{1}{\sin\left(\frac{\pi n}{L} z_s\right)} \frac{2\mu}{I_0^2}$$

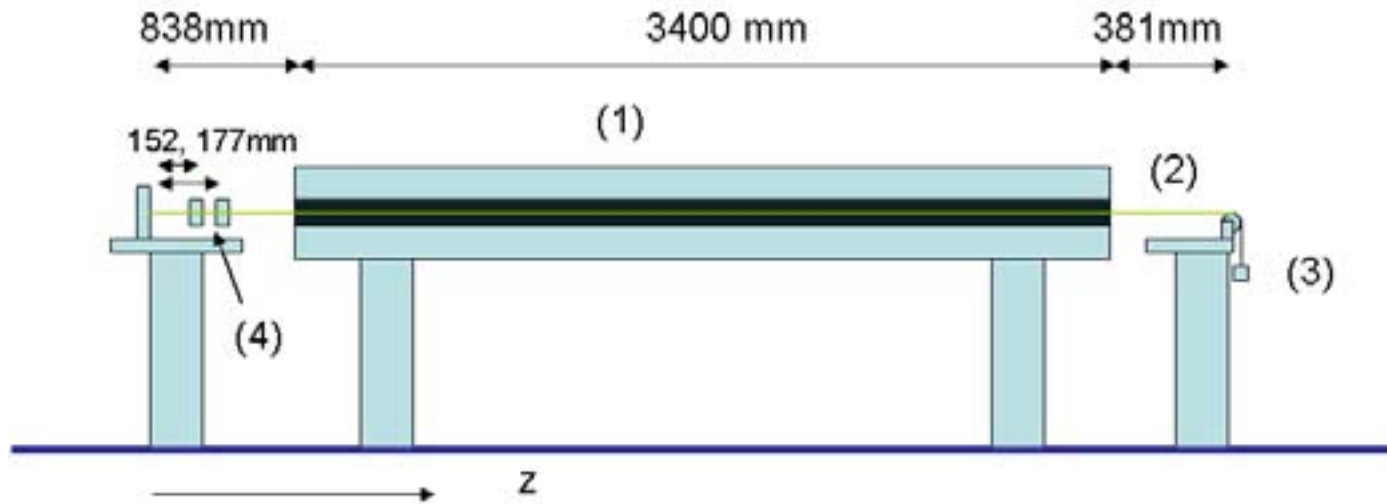
$$B_y(z) = \sum_{n=1}^{\infty} B_n \sin\left(\frac{\pi n}{L} z\right) \quad n \neq 2Nk \quad k = 1, 2, \dots$$



n	a(n)
1	6.76E+02
2	9.08E+02
3	-8.08E+02
4	-2.25E+03
5	-8.94E+02
6	1.82E+03
7	1.98E+03
8	-1.16E+02
9	-1.79E+03
10	-7.66E+02
11	4.83E+02
12	7.13E+02
13	7.62E+01



Experiment setup



1- LCLS undulator S/N 01, 2 – 100 μm copper-beryllium wire, 3 – load, 4 – LED phototransistor assemblies

Gap = 6.8mm

Period = 3.0 cm

Number of periods $N = 113$

Average peak field = 1.25T

The current amplitude = 100mA, driven directly by a wave form generator HP33120A

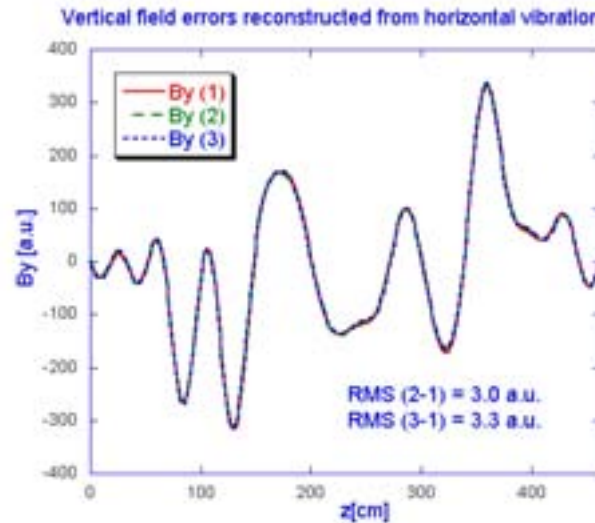
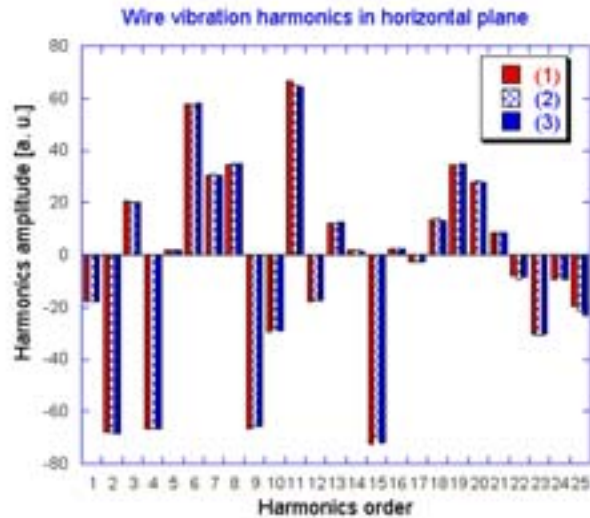
Signal recording by NI DAQcard – 6024E

Signals processed with LabView and MatLab programs

First vibration mode resonance frequency $\sim 30\text{Hz}$

Number of first modes scanned = 25

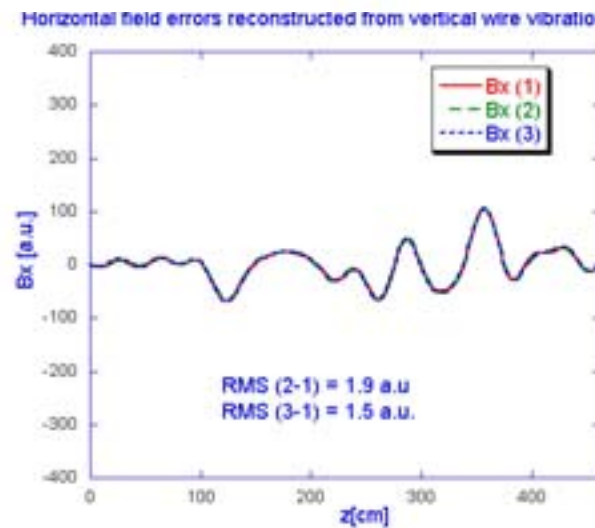
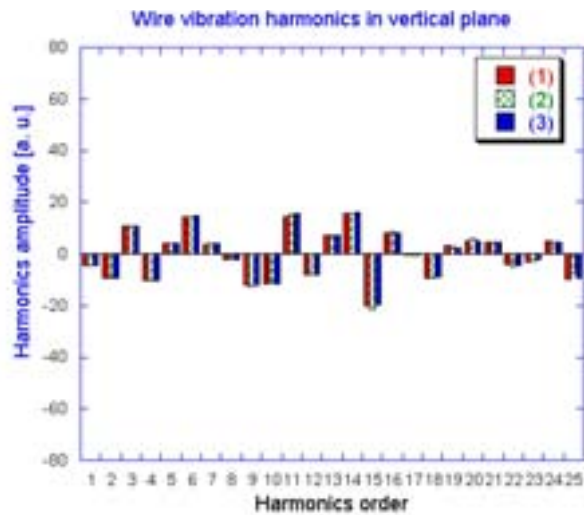
Repeatability test



1 and 2 measured within 1 hour,
3 – next day

25 harmonics used,
Shortest wavelength
~ 18cm or 6 periods

3 a.u. \approx 0.1G
 $\approx 10^{-5}$ of peak field



Field Integrals:

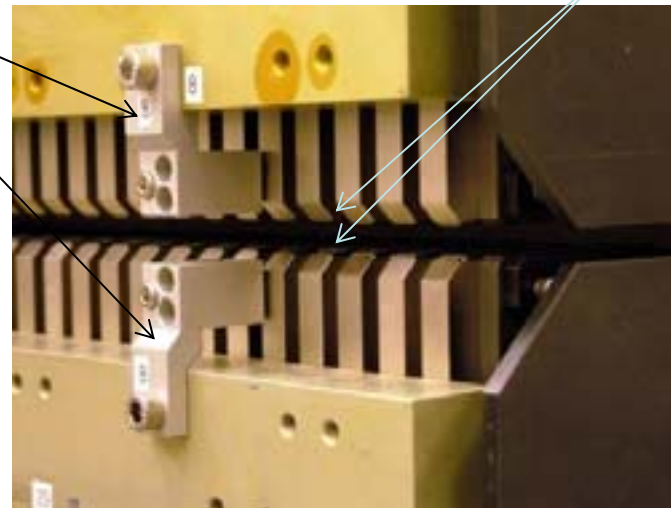
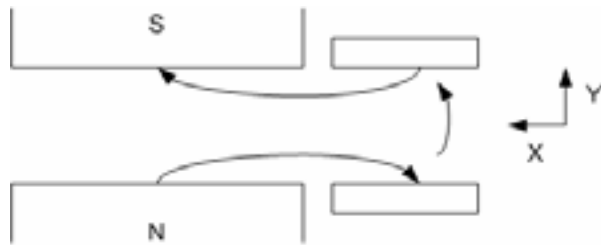
$I_{1y} = 114 \pm 2 \text{ G} \cdot \text{cm}$
 $I_{1x} = 2 \pm 1.2 \text{ G} \cdot \text{cm}$

Measurement of localized field distortion. Shims

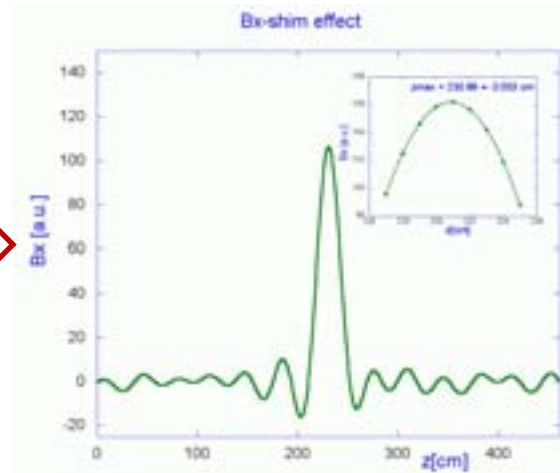
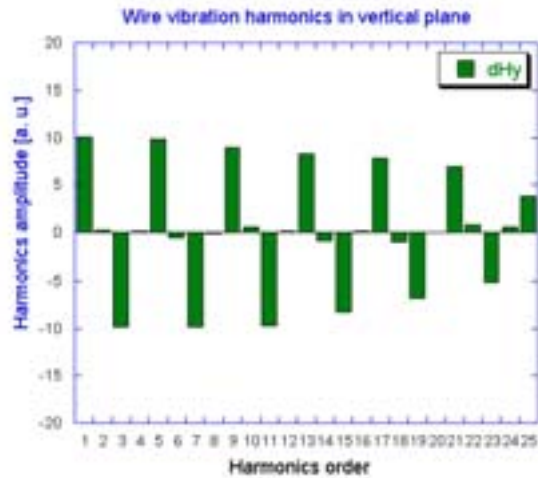
Y-field shims



X-field shims



Single shim measurement



Signal Calibration

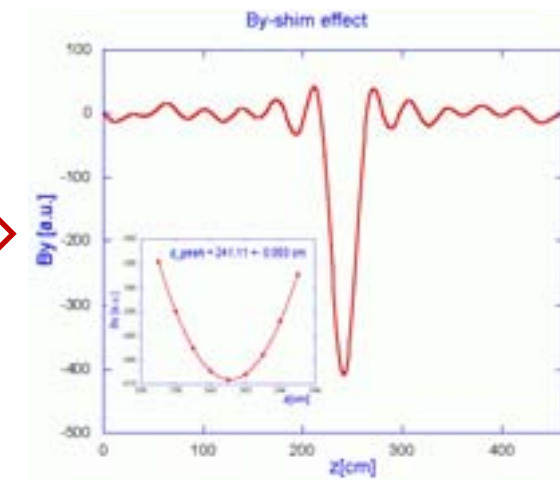
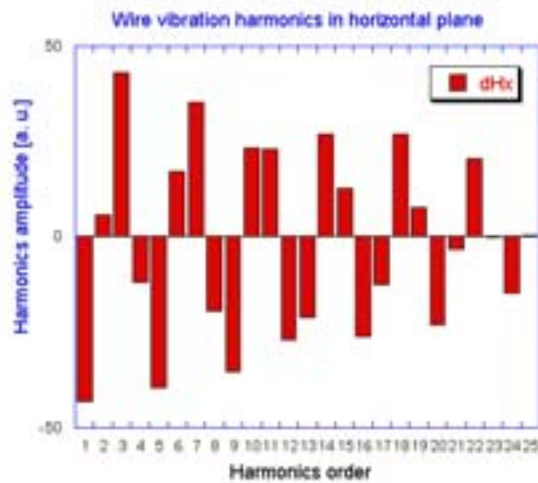
Peak area = 906 [a.u.·cm]

Field integral = 30 G·cm.

1 a.u. = 0.033 G

Shim location $z = 231\text{cm}$

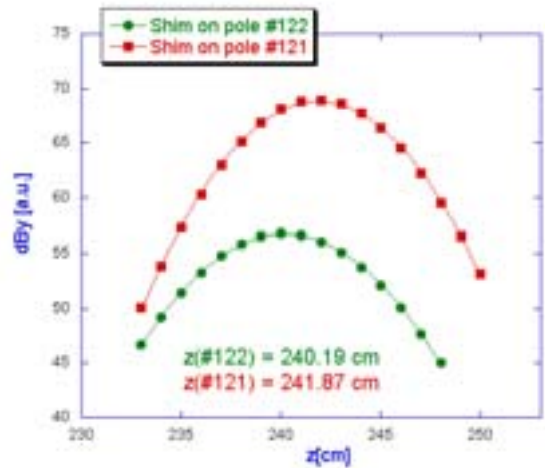
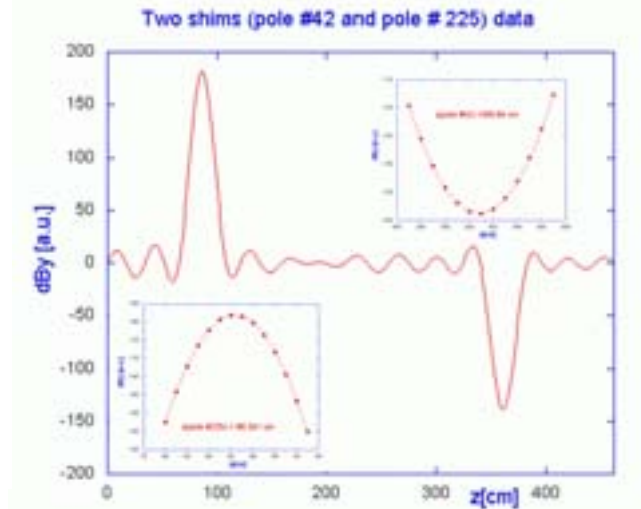
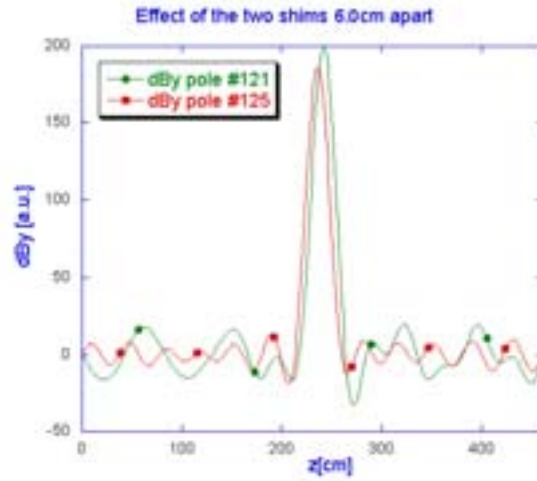
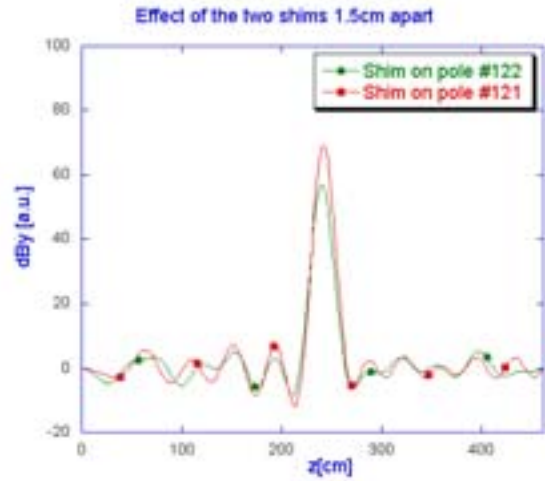
Measured $z = 230.89\text{cm}$



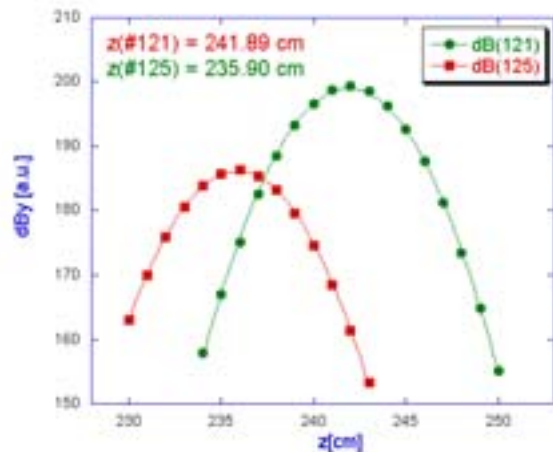
Shim location $z = 241\text{cm}$

Measured $z = 241.11\text{cm}$

Two shims measurement



2 shims 1.5 cm apart $\Delta z = 1.7$ cm



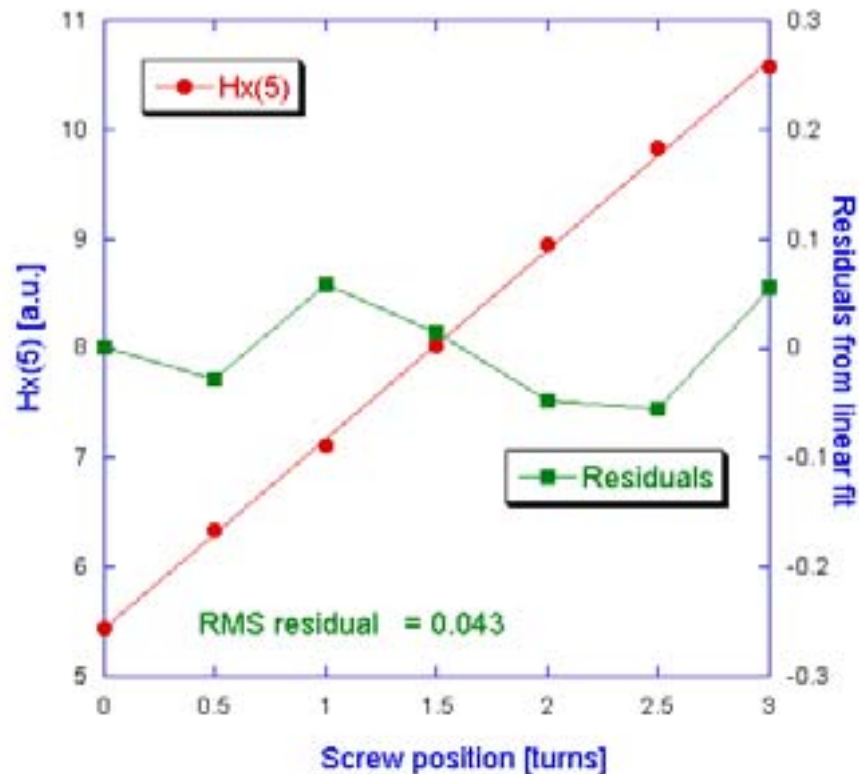
2 shims 6.0 cm apart $\Delta z = 6.01$ cm

2 shims 274.5 cm apart
 $\Delta z = 274.49$ cm between peaks



Sensitivity test

We varied strength of By shim and measured amplitude of the 5-th mode of wire vibration.



Calibration

From measurements of localized field distortion (see slide 8):

Field integral from shim = 340 G·cm

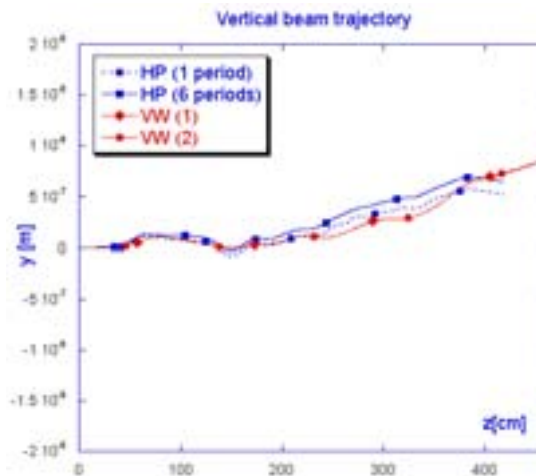
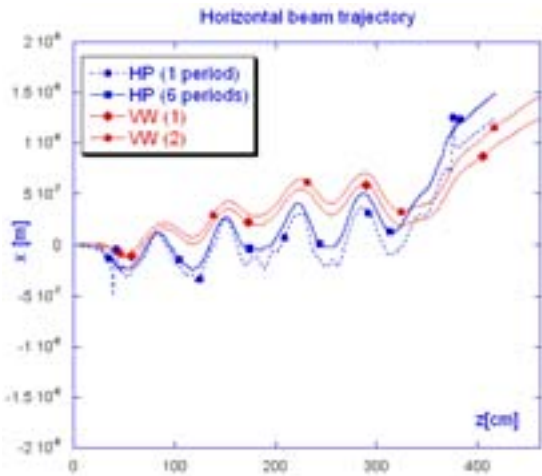
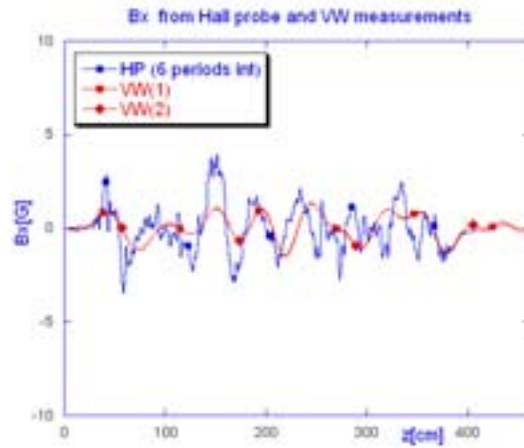
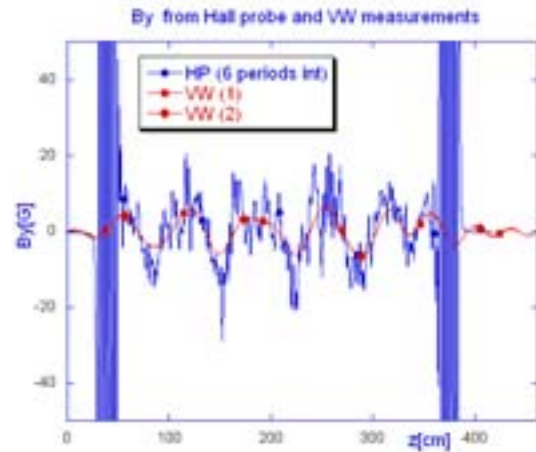
5th harmonic amplitude = 39 a.u.

1 a.u. = $340/39 \approx 9$ G·cm

Sensitivity (to local field change)

0.043 a.u. = 0.4 G·cm

Vibrating wire vs. Hall probe



Field Integrals
(Undulator S/N 13)

	I_y (G·cm)	I_x (G·cm)
VW	18 ± 3	15 ± 1
Hall Probe	21.0	18.0
Coil	6.0	21.0

Conclusion

The VW technique could be practical for:

- characterization of small gaps (bores) undulators and devices with limited access to the tested field region because of small sensor size.
- field integrals and beam trajectory tuning because of good space resolution (~ 1 mm), exceptional sensitivity to the local field integrals (~ 0.37 G cm) and acceptable accuracy of measuring field integrals over total magnet length (~ 6 G cm).
- adjustable phase and elliptical undulators tuning because of VW is free from effects analogous to the planar Hall effect.

The VW technique should be considered as a supplement to the Hall probe measurement because it cannot be used for the measurement and tuning of undulator parameter “K”.